

Divertor Design for Modification of JT-60 with Superconducting Coils

JAERI

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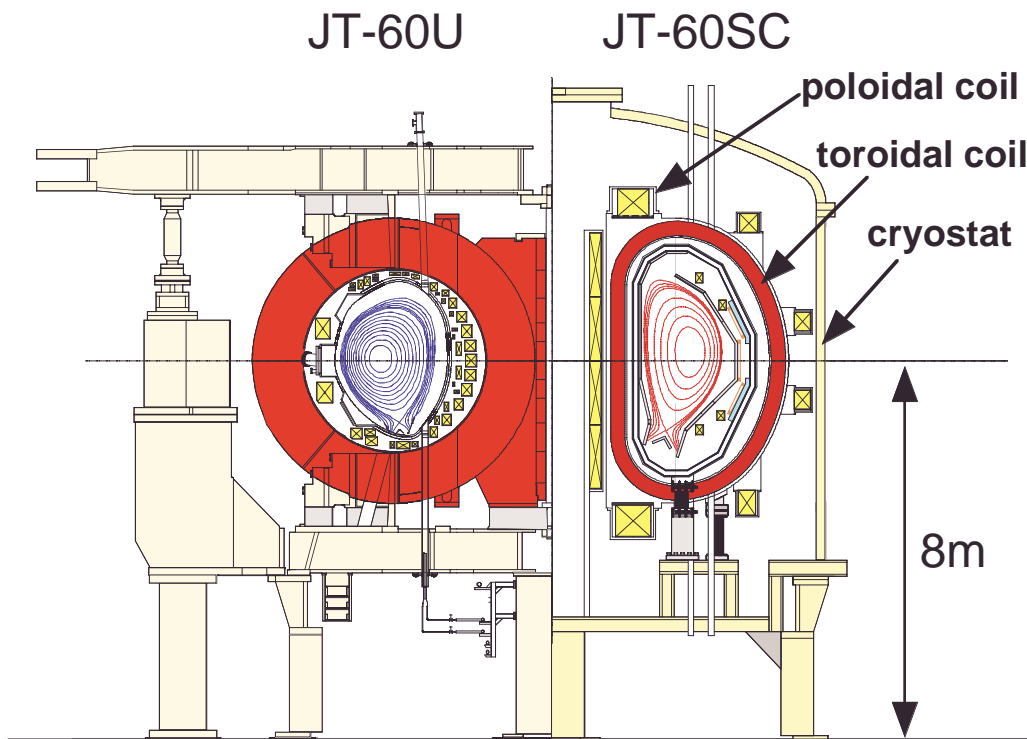
Summary

Main Objectives and Parameters of JT-60SC

to establish scientific and engineering bases for attractive DEMO reactor

- sustaining $\beta_N=3.5\sim 5.5$ longer than current skin time
- non-inductive full current drive with high bootstrap current fraction
- heat and particle control required for DEMO reactor
- feasibility study of a reduced activation ferritic steel for high β plasma

Existing facility (heating, power source, etc.) will be reused to reduce costs



Main Parameters

pulse width	100s
input power	44MW(10s) 30MW(30s) 25.4MW(50s) 14.7MW(100s)
plasma current	4MA
toroidal field	3.8T
major radius	2.8-3.0m
minor radius	0.7-0.9m
elongation κ_{95}	≤ 1.9
triangularity δ_{95}	≤ 0.45

Divertor research and development

Requirements of DEMO reactor

- Heat and particle control compatible with high β plasma
{radiation fraction $f_{\text{rad}} \geq 90\%$, partial detach, $\tau_{\text{He}^*} / \tau_E \leq 5$, density control}
- Low cost and long life-time plasma facing components

Time Table

basic phase

advanced phase

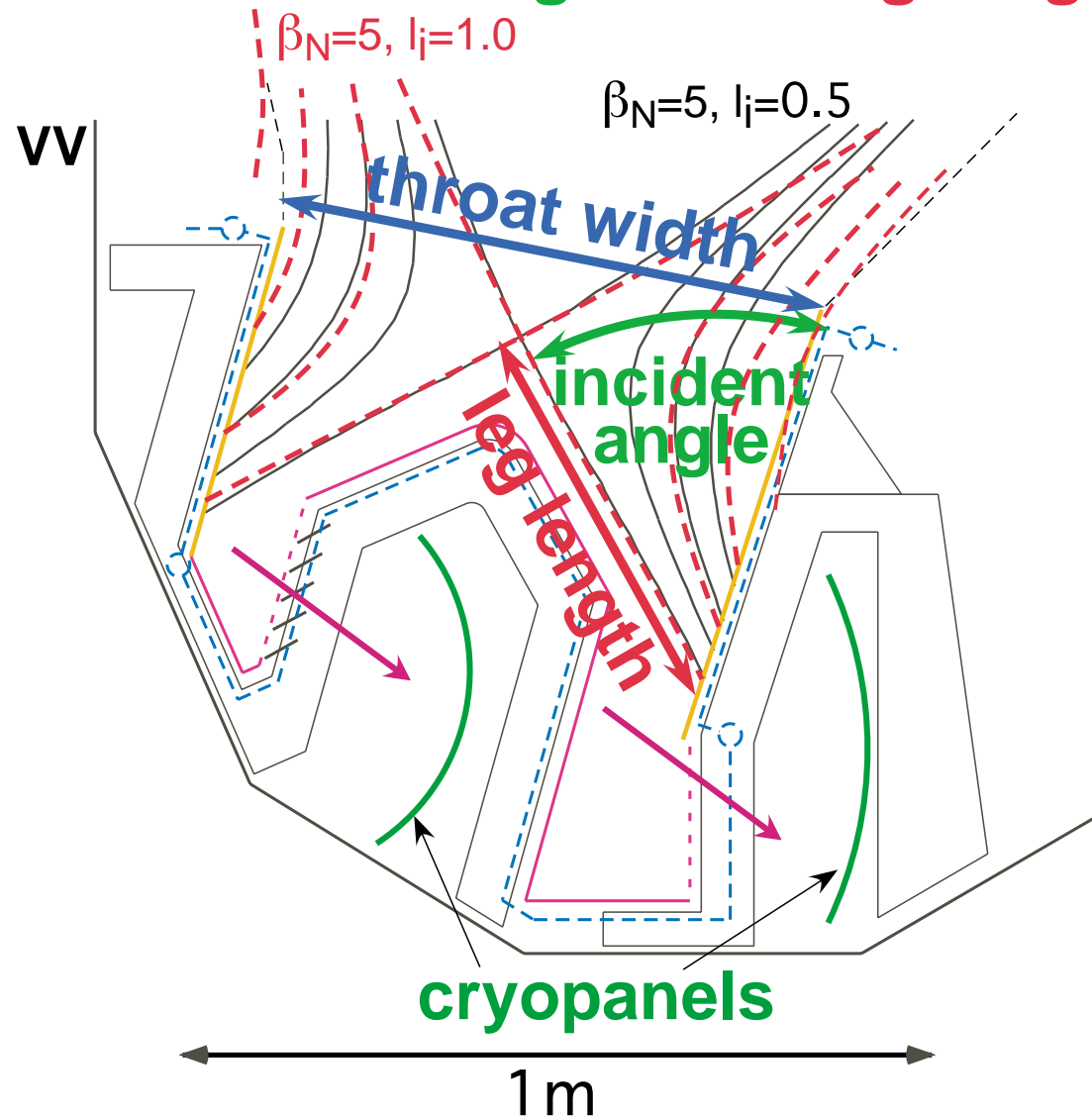
Main Objective β_N f_{rad}	compatibility with high β 3.5~5.5 (transient) $\geq 50\sim 65\%$	steady state, integration ≥ 3.5 (steady state) $\geq 80\%$
Divertor plasma PSI, PFC	Exhaust ($\geq 100\text{m}^3/\text{s}$) independent pumping at inner and outer divertor CFC ($10\sim 15\text{MW}/\text{m}^2$) test of metal by surface station	Geometry (full-closed) metal (long life-time)

Basic parameters of divertor geometry

Steps for design

1st : Throat width

2nd : Incident angle and Leg length

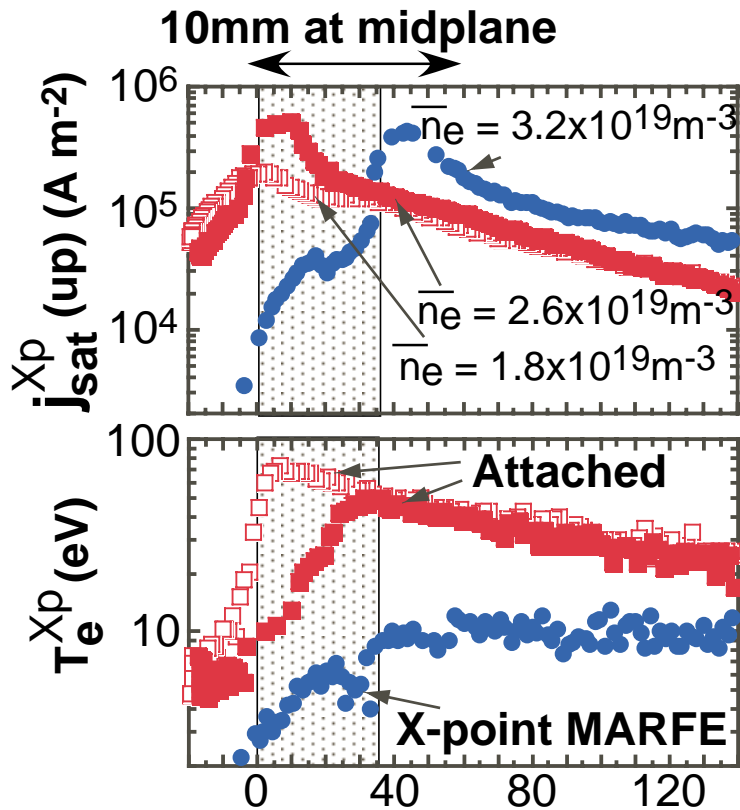


Requirements of baffle throat width

- Particle flux toward the divertor plate is broadened at X-point MARFE flux ($\propto nT^{0.5}$) decay length: **~15mm for attach**, **~10mm(shift)+~20mm for MARFE**
- Distance from separatrix to SOL flux surface increases with β_N and I_i .

Throat width is opened to 3cm SOL at $\beta_N \sim 5$ and $I_i = 1.0$

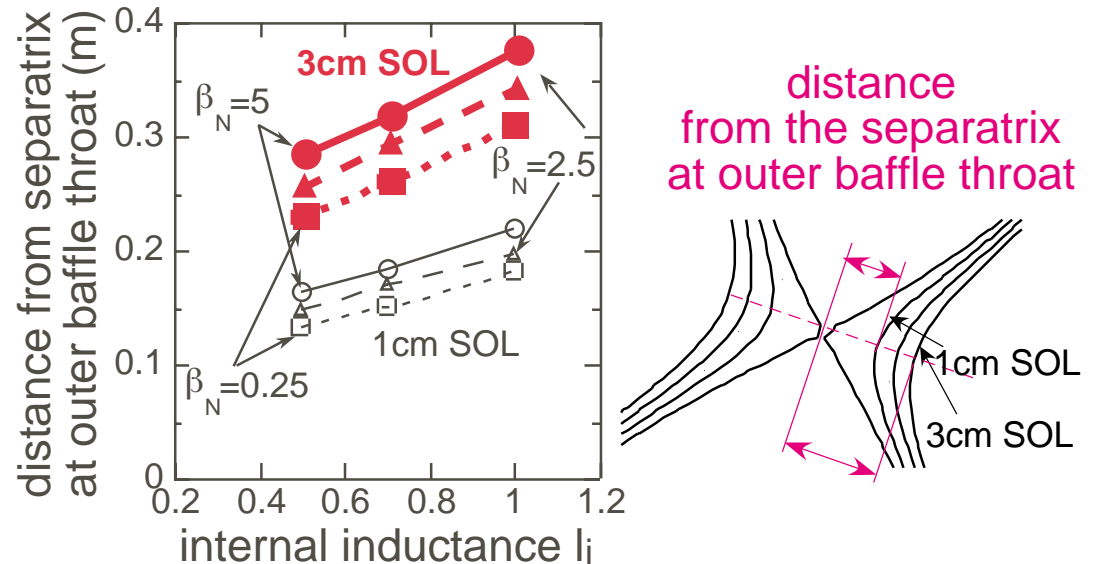
broadening of SOL particle flux



Distance from separatrix (mm)

just below the X-point in W-shaped divertor of JT-60U
ref. Nucl. Fus. 39, 1983-1994(1999)

expansion of SOL flux surface

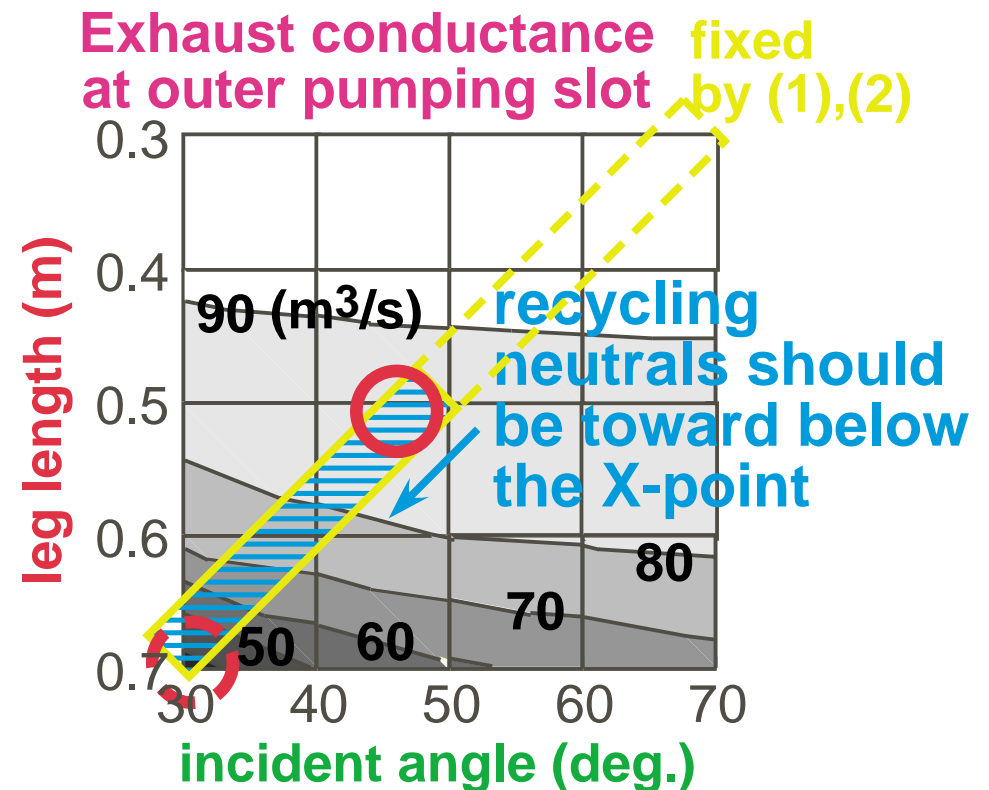
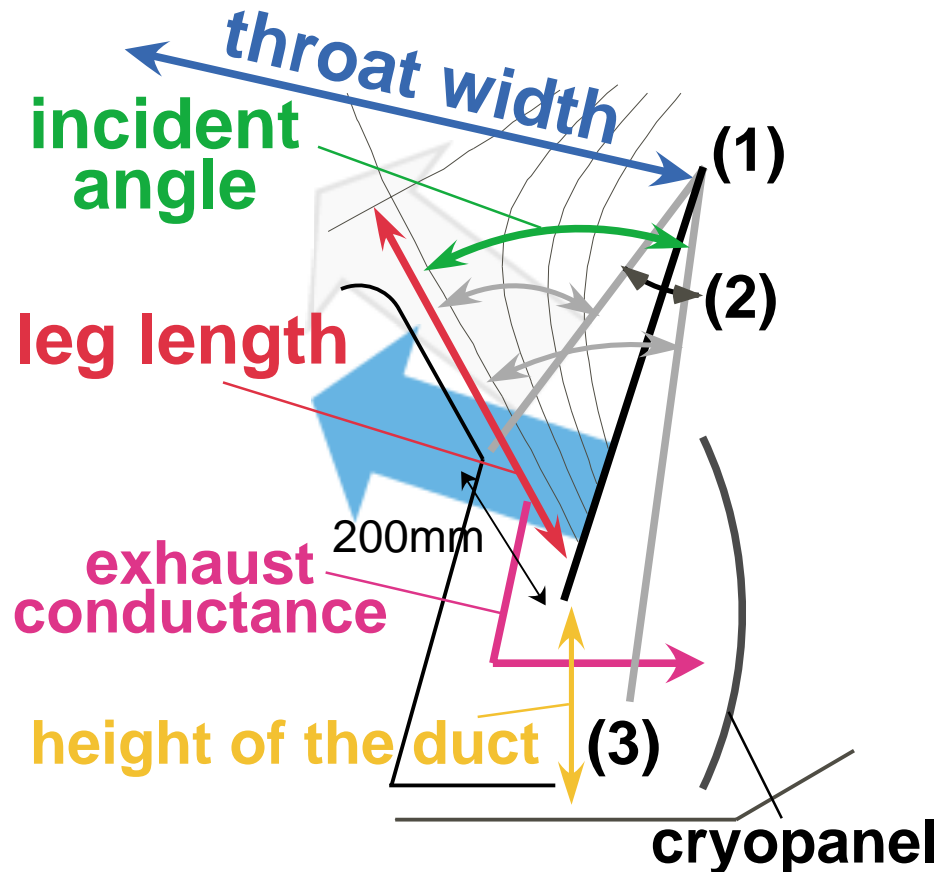


Incident angle and leg length

- (1) Top of the divertor plate is fixed by given **throat width**.
- (2) **Leg length** decreases as **incident angle** increasing.
- (3) Exhaust conductance mainly determined by **the height of the duct**.

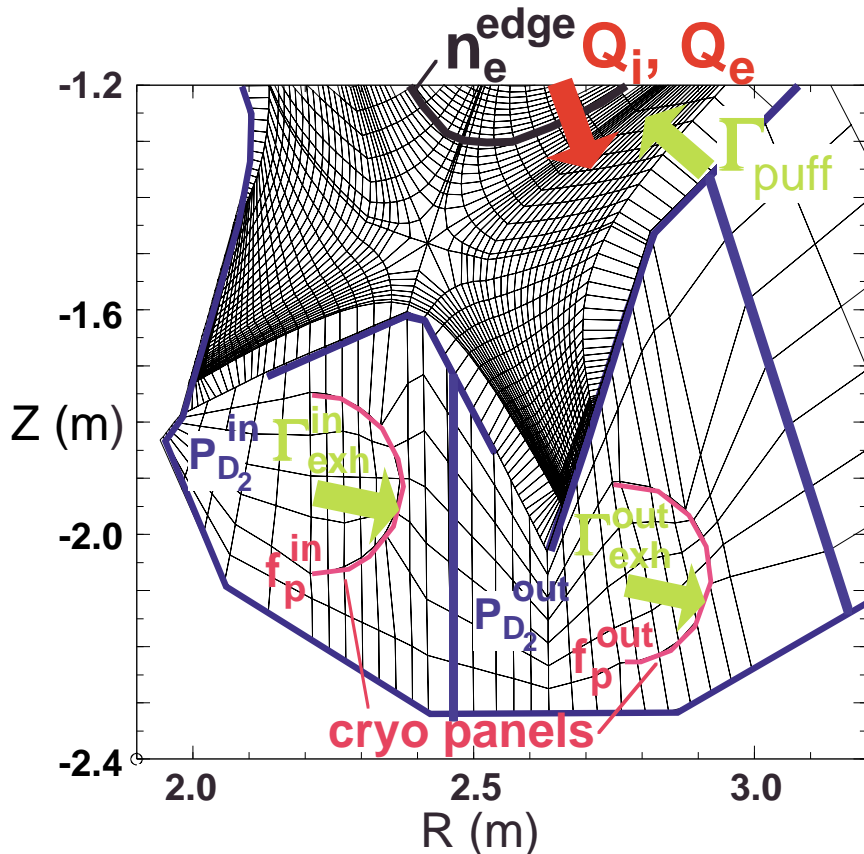
Exhaust conductance decreases from $85\text{m}^3/\text{s}$ to $35\text{m}^3/\text{s}$, when **leg length** increases 0.5m to 0.7m

0.5m is selected { \geq DIII-D (radiative outer leg) \gg JT-60U (W-shaped) }



Simulation of detachment control by pumping

- How large pumping speed is required to **sustain attachment or partial detachment** with avoiding MARFE onset?
- **Partially detached outer divertor** is simulated, and it **changes to attached by increasing exhaust probability** at cryopanel.
- **Effective pumping speed** of cryopanel are **evaluated from Γ_{exh} and P_{D2}** .



- Divertor fluid code (**SOLDOR**)
- 2D Monte Carlo code for neutral particle (**NEUT2D**)
- Impurity radiation is calculated by simplified non-corona model with **1.5% of carbon**

$n_{e\ edge} = 3.2 \times 10^{19} / m^3$

(corresponds to $f_{GW} \sim 0.7$ for $I_p = 1.5 \text{ MA}$)

Power flow to SOL : $Q_i = Q_e = 6 \text{ MW}$,

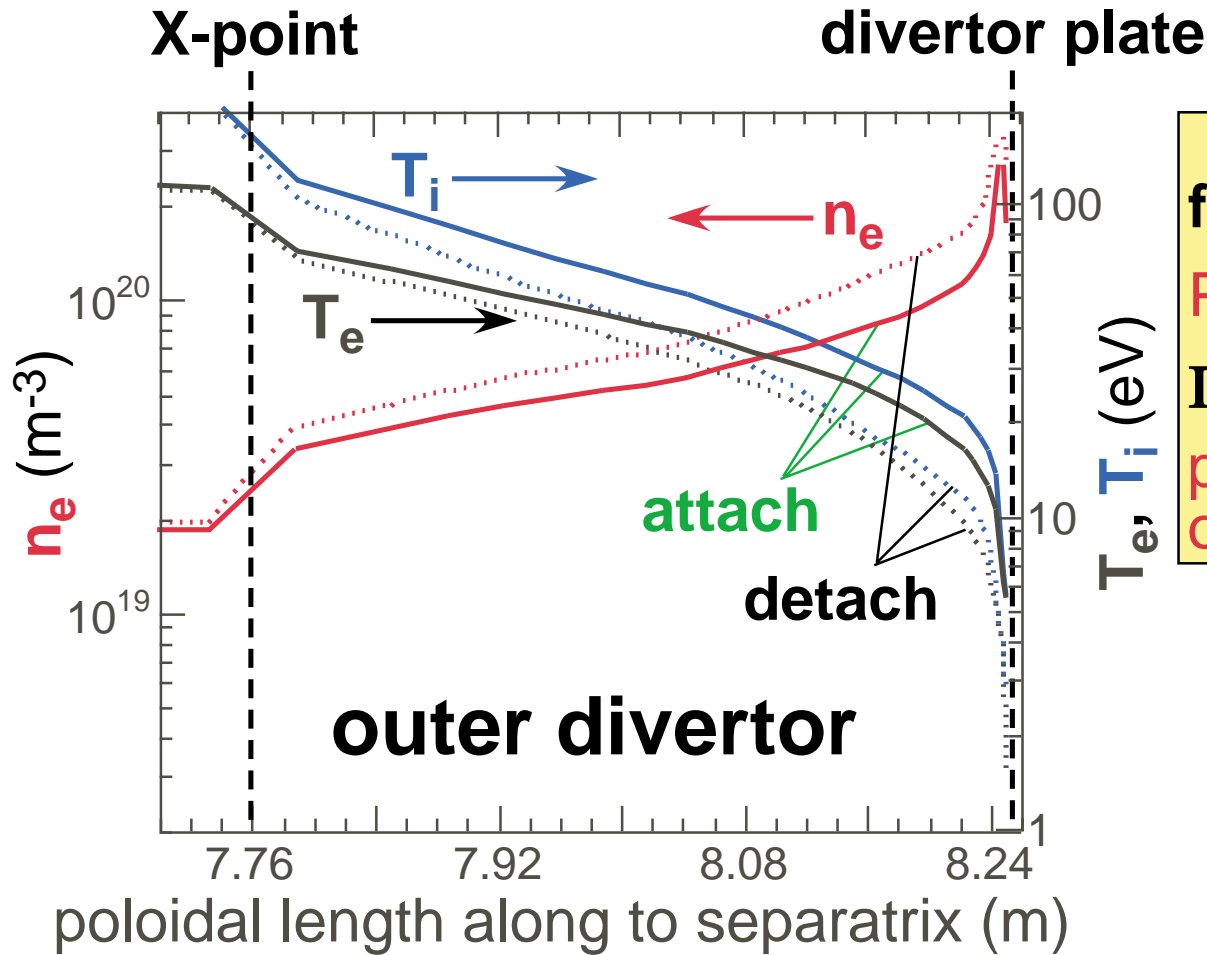
Gas puffing rate : $\Gamma_{puff} = 0.6 \times 10^{22} / s = 14.8 \text{ Pam}^3 / s$

f_p : **exhaust probability** at cryopanel,

Γ_{exh} : **exhausted flux**, P_{D2} : **neutral pressure**

Pumping speed for detachment control

- Pumping speed of outer cryopanel **required for the attached condition is evaluated to be 99m³/s.** It corresponds to **~42m³/s for pumping slot.**



	detach	attach
f_p^{in}/f_p^{out}	0.04/0.01	0.06/0.03
$P_{D_2}^{out}$ (Pa)	0.27	0.10
Γ_{exh}^{out} (Pam ³ /s)	5.4	9.9
pumping speed of cryopanel (m ³ /s)	20	99

Design of power handling

Feasibility for high β plasma research

input power : 30MW/30s ~ 15MW/100s

heat flux density is supposed to be **10~15MW/m²** at an allowable f_{rad} (50~65%) for high β plasma with input power of 30MW

Design of actively cooled divertor

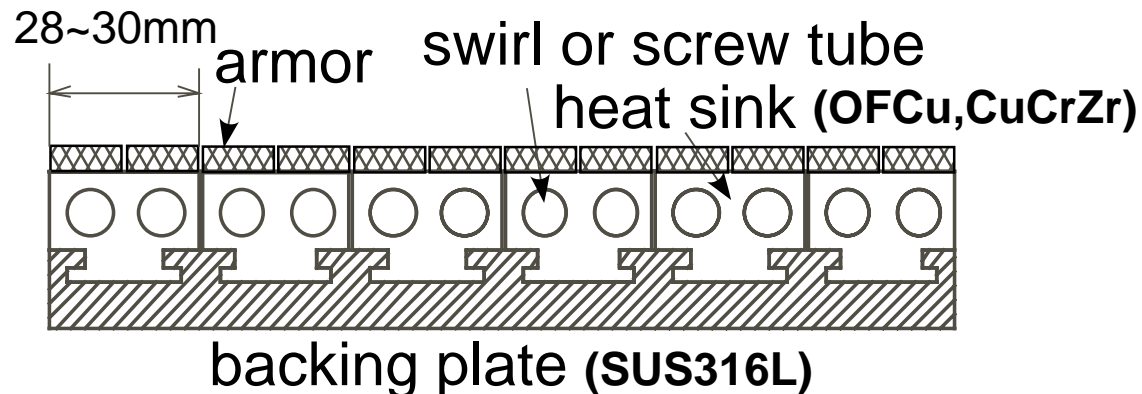
armor material : CFC for basic phase, W alloys for advanced phase

allowable surface temperature for steady heat flux :

~1000°C for CFC, ~700°C for W alloys (with keeping margin for ELMs)

typical thickness of armor : ~10mm for CFC, ≤ 5 mm for W alloys

development : Proto-type CFC target (40 x 40 x t10 mm) has survived for 1400 cyc. at 10MW/m².



Summary

- Basic divertor geometry is designed to obtain large exhaust conductance.
- Designed pumping speed ($\sim 200\text{m}^3/\text{s}$ at cryo panel) is enough to control detachment for outer divertor.
- Heat flux density $10\sim 15\text{MW}/\text{m}^2$ is supposed at outer divertor for the input power of 30MW with radiation fraction of $50\sim 65\%$.

Future Works

- Divertor geometry will be optimized by more detailed simulation. Effect of the incident angle and the leg length on the detached condition should be simulated.